

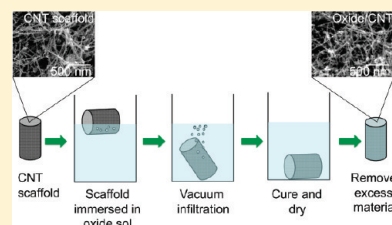
# Carbon Scaffolds for Stiff and Highly Conductive Monolithic Oxide–Carbon Nanotube Composites

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**ABSTRACT:** The ultra low density, high electrical conductivity, and mechanical robustness of carbon nanotube aerogels (SWNT-CA) make them ideal scaffolds around which to create novel composites. Here we report on the synthesis and characterization of oxide/carbon nanotube composites fabricated through the sol–gel deposition of oxide coatings ( $\text{SiO}_2$ ,  $\text{SnO}_2$  or  $\text{TiO}_2$ ) on SWNT-CA. The porous network of the SWNT-CA scaffold is retained after the deposition and drying process. In each case, the deposited oxide appears to form a uniform coating on the surfaces of aerogel ligaments. The composite materials exhibit high electrical conductivity ( $\sim 100$  S/m) and enhanced mechanical properties relative to the uncoated SWNT-CA support. In addition, the oxide/SWNT-CA composites possess high surface areas (as high as  $742$   $\text{m}^2/\text{g}$ ) and large mesopore volumes (as high as  $2.2$   $\text{cm}^3/\text{g}$ ). This approach offers viability in engineering new oxide/CNT composites for applications such as energy storage, sensing, and catalysis.

**KEYWORDS:**



## INTRODUCTION

Nanocomposites of carbon nanotubes (CNTs) and various oxides<sup>1</sup> are among the most researched functional materials because of their many extraordinary properties in electronic,<sup>2–8</sup> storage,<sup>9–13</sup> structural,<sup>14–17</sup> catalytic,<sup>18–23</sup> and sensing<sup>24–27</sup> applications. The range of composites fabricated covers many oxides, and the methods for combining the oxides and CNTs include mechanical mixing, sol–gel coating, chemical and physical vapor deposition, hydrothermal methods, and more.<sup>1</sup> Although much of the existing research involves the use of loose CNT powder or vertical CNT arrays in the preparation of the nanocomposite, a number of technologies would benefit from the design of composites from free-standing three-dimensional (3D) monoliths of interconnected CNTs.<sup>4,5,9,19</sup> For example, in battery applications composite powders or arrays typically require addition of significant amounts of nonactive material (binder, metal conductor, or a metal substrate to support the array) to create a working electrode. Alternatively, integration of the active material into a mechanically robust and electrically conductive 3D CNT scaffold structure would eliminate the need for the nonactive material, greatly increasing the energy density of the system. Furthermore, if the 3D CNT assembly were both scalable and possessed isotropic mechanical stability, in contrast to vertical CNT arrays which are limited to millimeters in height and possess anisotropic properties, it would be amenable to a greater number of different deposition methods (solution- or gas-phase) and significantly improve versatility in the design and manufacturing for many applications.

We recently reported on a new class of ultra low-density single-wall CNT-based carbon aerogels (SWNT-CA) that are comprised of randomly oriented CNTs cross-linked by sol–gel

derived graphitic carbon nanoparticles.<sup>28</sup> These materials exhibit high electrical conductivity and robust mechanical properties at densities as low as  $10$   $\text{mg}/\text{cm}^3$  without additional reinforcement. In addition, the SWNT-CAs are structurally stable across temperatures ranging from a few Kelvin to over  $1700$  K (inert atmosphere) and can be fabricated as conformable monoliths with macroscopic dimensions. Therefore, these materials serve as attractive platforms for the fabrication of new monolithic CNT composite structures. We previously demonstrated the utility of these SWNT-CAs as scaffolds in the preparation of nonporous polymer/SWNT-CA composites with extraordinary electrical conductivity and mechanical properties.<sup>29</sup> In these composite structures, the free pore volume of the SWNT-CA is completely filled with polymer through direct infiltration of the monolithic support. These materials, with as little as  $1$  vol% of the SWNT-CA support, exhibited a 3-fold improvement in elastic modulus compared to the polymer alone. The electrical conductivity of the composite was also high ( $100$  S/m), indicating that the network structure of the SWNT-CA was sufficiently robust to handle infiltration and curing of the polymer. Extension of this approach to other classes of materials, such as oxide/CNT composites, would provide strong evidence for the potential of the 3D SWNT-CA scaffold in the design of new nanocomposite structures.

In the work presented here, we describe the fabrication of novel oxide/SWNT-CA composites through the sol–gel deposition of oxides on the surface of nanoligaments of SWNT-CA monoliths. Unlike the nonporous polymer/SWNT-CA

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composites, the oxide is deposited as a conformal overlayer on the primary ligament structure of the SWNT-CA support, thus preserving open porosity within the monolithic part. This work specifically focuses on nanoporous composites prepared with  $\text{SiO}_2$ ,  $\text{SnO}_2$  and  $\text{TiO}_2$  coatings due to the technological interest in each of these materials. In particular, composites of  $\text{SiO}_2$  and CNTs<sup>30–33</sup> possess desirable properties for a wide range of applications such as electrochemical devices,<sup>34</sup> catalysis,<sup>35</sup> sensors,<sup>25</sup> optoelectronics<sup>8</sup> and separations.<sup>36</sup>  $\text{SnO}_2$ /CNT composites<sup>37</sup> have shown potential as sensors,<sup>24,26</sup> catalyst supports,<sup>18,21</sup> and Li-ion battery electrodes,<sup>10,13,23,38–41</sup> whereas  $\text{TiO}_2$ /CNT composites<sup>6,31,32,42</sup> are of interest because of their potential impact in fields of catalysis,<sup>23,43–45</sup> photoelectronics,<sup>5</sup> and energy storage.<sup>11,46</sup> Structural characterization of the oxide/SWNT-CA composites shows that, in each case, sol–gel deposition of the oxide coating occurs primarily on the surfaces of CNT ligaments throughout the aerogel monolith. In addition, these composite structures retain the high electrical conductivity of the SWNT-CA support and exhibit significant enhancements in mechanical properties relative to the uncoated aerogel structure. The approach described here provides a straightforward route to the design of porous and monolithic oxide/CNT composites for use in a variety of applications.

## ■ EXPERIMENTAL SECTION

**Oxide/SWNT-CA Composite Preparation.** The SWNT-CA nanoporous supports, with a SWNT loading of 55 wt % of solids (1 vol%) and a monolith density of 30 mg/cm<sup>3</sup>, were prepared as previously described.<sup>28</sup> The oxide/SWNT-CA composites were prepared through deposition of an oxide coating over the inner surface area of the SWNT-CA framework using sol–gel chemistry. The oxide sol–gel solutions were also synthesized using literature methods.<sup>47–49</sup> The  $\text{SiO}_2$  sol–gel was prepared via traditional one-step base-catalyzed alkoxide sol–gel chemistry using tetramethoxysilane (4.1 g), water (1.5 g), ammonium hydroxide (30%, 200  $\mu\text{L}$ ), and methanol (24 g).<sup>49</sup> The  $\text{TiO}_2$  sol–gel was prepared via a two-step process involving acid-catalyzed hydrolysis of titanium(IV) ethoxide (1 g) using water (85.7  $\mu\text{L}$ ), hydrochloric acid (37%, 71.4  $\mu\text{L}$ ), and ethanol (3.57 g), followed by base-initiated gelation using propylene oxide (0.357 g).<sup>47</sup> The  $\text{SnO}_2$  sol–gel was prepared via an epoxide-initiated gelation method using tin chloride pentahydrate (0.56 g), trimethylene oxide (1.03 g), ethanol (7 g), and water (5 g).<sup>48</sup> Composites were synthesized by infiltration of SWNT-CA monoliths by the oxide sol–gel solutions prior to gelation. The SWNT-CA's were immersed in the sol–gel solutions and placed under vacuum until no more air escaped from the scaffolds, indicating full penetration of the sol. The concentration of inorganic precursors was kept low to promote the growth of the condensed inorganic phase primarily on the surfaces of the SWNT-CA framework, while minimizing gelation in the free pore volume of the aerogel. The infiltrated SWNT-CAs were then cured at room temperature for 72 h to produce the wet oxide/SWNT-CA gels. The wet oxide/SWNT-CA gels were dried using supercritical extraction with liquid  $\text{CO}_2$  to yield the final dry oxide/SWNT-CA composites.

**Characterization.** Bulk densities of the samples were determined from the physical dimensions and mass of each sample. The volume percent of CNT in each sample was calculated from the initial mass of SWNTs added, with an assumption of a CNT density<sup>50</sup> of 1.6 g/cm<sup>3</sup>, and the final volume of the aerogel. Scanning electron microscopy (SEM) characterization was performed on a JEOL 7401-F at 5–10 keV in secondary electron imaging mode with a working distance of 2–8 mm. Due to good electrical conductivity of the CNT scaffold, no conductive coating of specimens was required before SEM imaging.

Transmission electron microscopy (TEM) characterization was performed on a Phillips CM-300FEG electron microscope operated at 300 kV. Samples for TEM were prepared by pulverizing aerogels above TEM grids. Surface area determination and pore volume and size analysis were performed by Brunauer–Emmett–Teller (BET) and Barrett–Joyner–Halenda (BJH) methods using an ASAP 2010 Surface Area Analyzer (Micromeritics Instrument Corporation).<sup>51</sup> Samples of approximately 0.1 g were heated to 150 °C under vacuum ( $10^{-5}$  Torr) for at least 24 h to remove adsorbed species prior to analysis. Ultraviolet–visible (UV–vis) absorption spectroscopy was performed on a Perkin-Elmer Lambda 950. Samples for UV–vis analysis were prepared by suspension of pulverized material in ethanol via ultrasonication. The titania contribution curve was generated by subtracting the raw SWNT-CA spectrum from the raw  $\text{TiO}_2$ /SWNT-CA spectrum. No scaling was necessary as the background signals from both aerogels were of the same intensity.

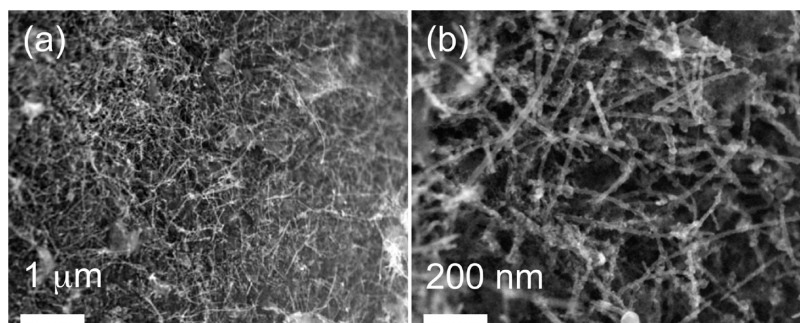
Powder X-ray diffraction (XRD) analysis of the samples was performed with  $\text{Cu K}\alpha$  radiation on a Scintag PAD-V X-ray diffractometer. Rutile  $\text{TiO}_2$  powder was used as a standard. Oxide content was determined using thermogravimetric analysis (TGA) performed on a Shimadzu TGA 50 Thermogravimetric Analyzer. Samples were heated in air to 1000 °C at 10 °C/min in alumina boats. The residual mass was considered the oxide content. Electrical conductivity was measured using the four-probe method with metal electrodes attached to the ends of cylindrical samples. The amount of current transmitted through the sample during measurement was 100 mA, and the voltage drop along the sample was measured over distances of 3–6 mm. Seven or more measurements were taken on each sample, and results were averaged.

Mechanical properties were studied by indentation in an MTS XP Nanoindenter with a spherical sapphire indenter with a radius of 496  $\mu\text{m}$ . Before indentation, aerogel monoliths were attached to silicon wafers with epoxy. A series of both continuous and partial load-unload indents (with an unloading percentage of 100%) was carried out under ambient conditions. The loading rate was continuously adjusted to keep a constant representative strain rate of  $1 \times 10^{-3} \text{ s}^{-1}$ , as discussed previously.<sup>52</sup> Young's modulus was calculated according to the method of Oliver and Pharr.<sup>53</sup> We assume Poisson's ratios of sapphire and aerogels of 0.23 and 0.20, respectively, and the Young's modulus of sapphire of 425 GPa.<sup>52</sup> For each specimen, from 8 to 12 measurements were taken from different locations, and results were averaged. Error bars given in the tables for the Young's modulus are the standard error in the mean.

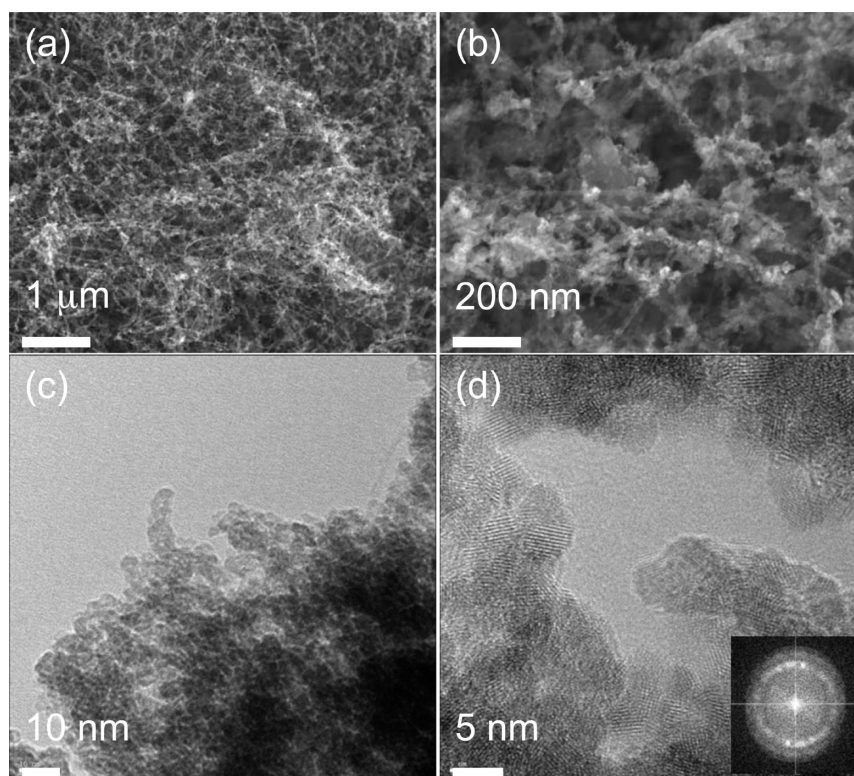
## ■ RESULTS AND DISCUSSION

Examination of the composite structures by SEM (Figures 1–2) shows that the porous network structure of the SWNT-CA support is maintained after the oxide deposition and drying process. Additionally, in each case, the deposited oxide appears to form a uniform coating on the surfaces of the CNT ligaments. For example, the SEM images for the  $\text{SiO}_2$ /SWNT-CA composite show that the deposited  $\text{SiO}_2$  aerogel particles preferentially coat the CNT bundles, as very few unsupported  $\text{SiO}_2$  particles were observed (Figure 1a,b). Similarly, the SEM images for the  $\text{SnO}_2$ /SWNT-CA show that the majority of  $\text{SnO}_2$  particles are associated with the CNT network (Figure 2). Unlike the  $\text{SiO}_2$  composite, however, the deposited  $\text{SnO}_2$  particles are crystalline with diameters of  $\sim 3$ –5 nm, consistent with previous reports for  $\text{SnO}_2$  aerogels prepared using a similar sol–gel formulation.<sup>48</sup> The  $\text{TiO}_2$  particles, as deposited, are amorphous but can be converted to the anatase phase after calcination at 320 °C for 5 h in air, as indicated by XRD (Figure 3). After annealing, the  $\text{TiO}_2$  nanocrystals are easily distinguishable by both SEM and TEM





**Figure 1.** SEM images of SiO<sub>2</sub>/SWNT-CA composites at (a) low and (b) high magnifications.



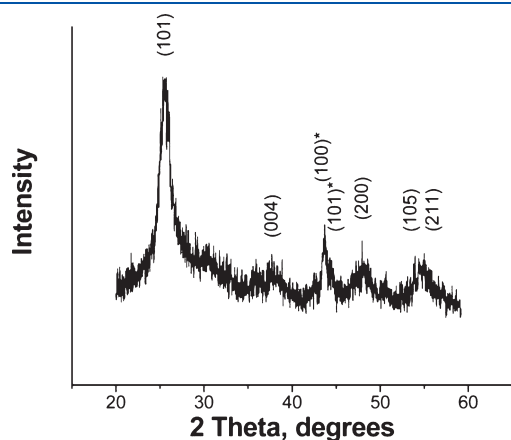
**Figure 2.** SEM images of SnO<sub>2</sub>/SWNT-CA composites at (a) low and (b) high magnifications. TEM images of SnO<sub>2</sub>/SWNT-CA composites at (c) low and (d) high magnification. Inset in (d) is the electron diffraction pattern of the SnO<sub>2</sub>/SWNT-CA.

from the underlying support structure (Figure 4). The electron diffraction pattern (the inset in Figure 4f) further confirms the crystalline nature of the TiO<sub>2</sub> particles after annealing.

Not surprisingly, the gas adsorption properties of the oxide/SWNT-CA composites are quite different from those of the uncoated support material. As shown in Figures 5–7, the nitrogen isotherms for these composite structures are consistent with materials comprised of both meso- and macropores. Because the SWNT-CA support is primarily a macroporous structure, the mesoporosity in these materials can be attributed to the porous oxide coating. Each of the composite structures exhibits larger surface area and mesopore volume than those respective values for the SWNT-CA support, which are similar to surface areas observed in pure metal oxide aerogels.<sup>47–49,54,55</sup> Notably, the BET surface area (742 m<sup>2</sup>/g) and mesopore volume (2.2 cm<sup>3</sup>/g) measured for the SiO<sub>2</sub>/SWNT-CA composite are

considerably larger than the values measured for the SWNT-CA support (162 m<sup>2</sup>/g, 0.3 cm<sup>3</sup>/g) and on par with values observed in the pure SiO<sub>2</sub> aerogel (670 m<sup>2</sup>/g, 1.8 cm<sup>3</sup>/g). This change in textural properties has been observed with other SiO<sub>2</sub>/CNT composites.<sup>36</sup> The SnO<sub>2</sub> composite also exhibits significant increases in BET surface area (349 m<sup>2</sup>/g) and mesopore volume (0.9 cm<sup>3</sup>/g) relative to the support structure. Interestingly, the crystalline TiO<sub>2</sub>/SWNT-CA composite has a greater mesopore volume than the amorphous composite (1.1 vs 0.6 cm<sup>3</sup>/g), whereas the BET surface areas remain similar (197 and 202 m<sup>2</sup>/g for crystalline and amorphous composites, respectively). Thus, crystallization of the deposited TiO<sub>2</sub> particles was achieved without loss of accessible surface area. The high surface areas and large mesopore volumes associated with these composite materials would be expected to be beneficial for energy storage, catalyst, and sensing applications.

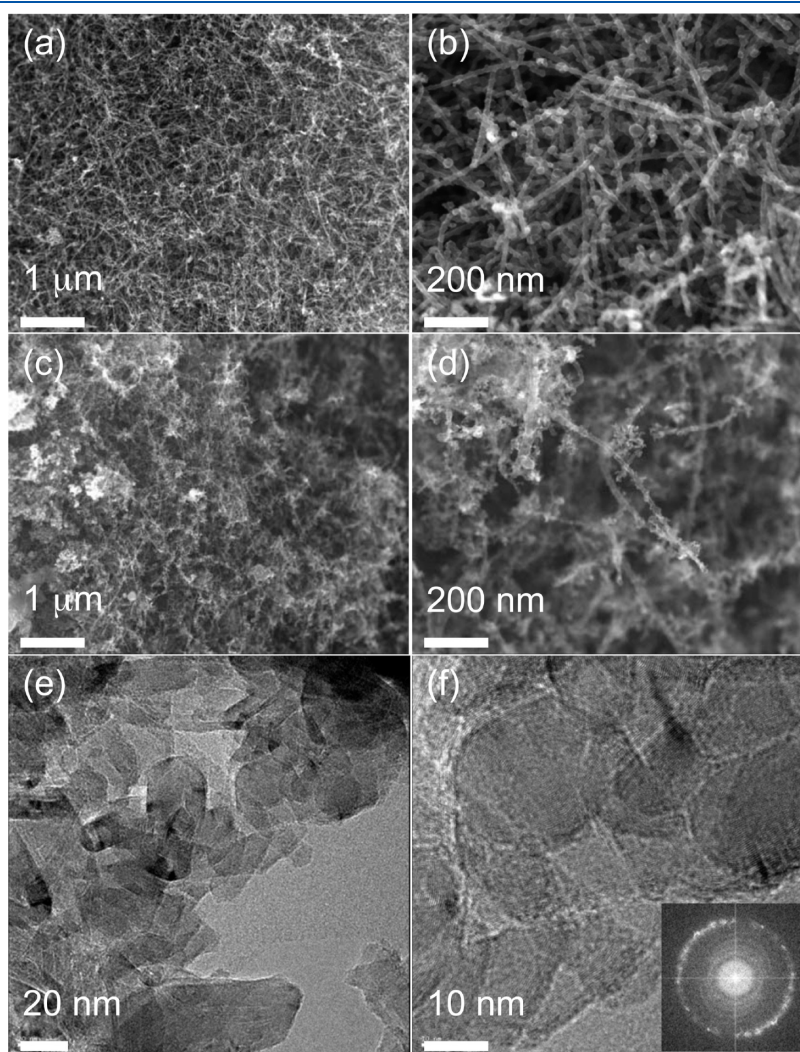
Structural integrity and electrical conductivity are also important considerations in designing porous structures for use as



**Figure 3.** Powder X-ray diffraction spectrum for a  $\text{TiO}_2$ /SWNT-CA composite annealed at 320 °C. Asterisks indicate peaks indexed to graphite. All other peaks indexed to anatase phase  $\text{TiO}_2$ .

catalyst supports and electrodes. Therefore, the mechanical and electrical properties of the composite structures were evaluated (Tables 1 and 2 and Figure 8). The electrical conductivities of each of the oxide-coated composites are similar to that of the uncoated SWNT-CA structure, suggesting that the conductive CNT network is intact after deposition and supercritical drying. This observation is consistent with our previous results for polymer/SWNT-CA composites.<sup>29</sup>

Mechanical properties of the composites show a more complex behavior than that of electrical conductivity. For example, Figure 8 compares continuous load–displacement curves for a  $\text{SiO}_2$ /SWNT-CA composite, a  $\text{SiO}_2$  aerogel, and a SWNT-CA scaffold. It is seen from Figure 8 that, for the maximum load used, the deformation of the SWNT-CA scaffold is purely elastic with a modulus of 1.2 MPa (Table 1). This is consistent with our previous report.<sup>28</sup> In contrast, the deformation of the silica aerogel has a large inelastic component, which is evidenced by a difference in loading and unloading curves and a large residual displacement of  $\sim 30\ \mu\text{m}$ . This behavior is in contrast to an almost entirely elastic deformation of TMOS-derived base-catalyzed  $\text{SiO}_2$  aerogels prepared slightly differently and reported previously.<sup>52</sup> All three oxide aerogels studied in the present work (silica, titania, and



**Figure 4.** SEM images of (a, b) as-synthesized and (c, d) annealed at 320 °C  $\text{TiO}_2$ /SWNT-CA composites at low and high magnifications. TEM images of annealed (e, f)  $\text{TiO}_2$ /SWNT-CA composites at low and high magnifications. Inset in (f) is the electron diffraction pattern of the annealed  $\text{TiO}_2$ /SWNT-CA.

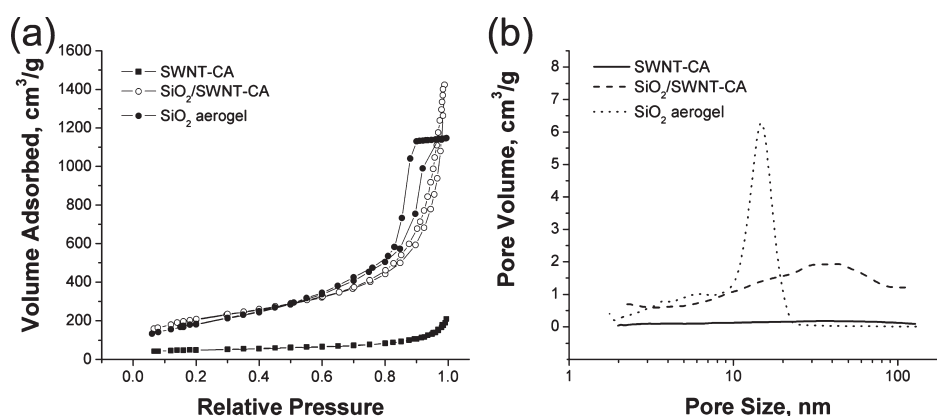


Figure 5. Plots of the (a) nitrogen adsorption/desorption isotherms and (b) pore size distribution for SiO<sub>2</sub>/SWNT-CA, SWNT-CA, and bulk SiO<sub>2</sub>.

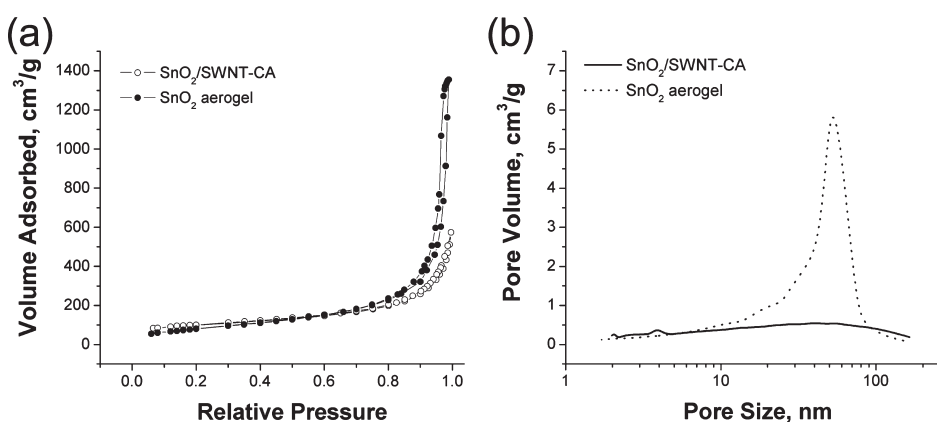


Figure 6. Plots of the (a) nitrogen adsorption/desorption isotherms and (b) pore size distribution for SnO<sub>2</sub>/SWNT-CA and bulk SnO<sub>2</sub>.

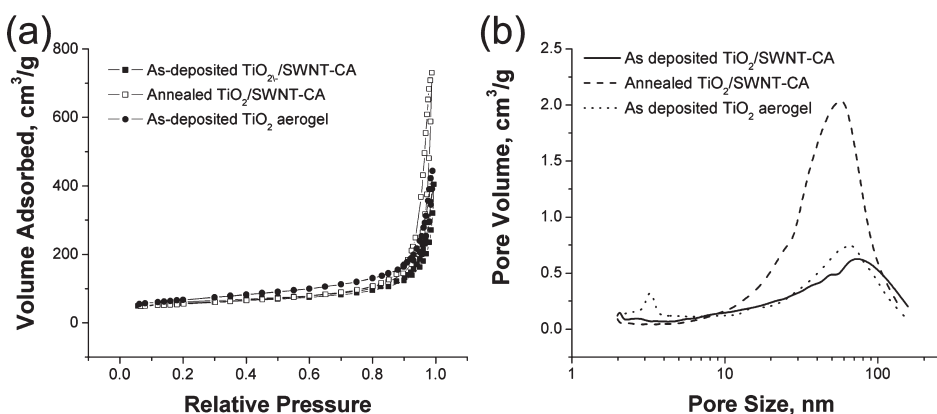


Figure 7. Plots of the (a) nitrogen adsorption/desorption isotherms and (b) pore size distribution for TiO<sub>2</sub>/SWNT-CA (as-deposited and annealed) and bulk TiO<sub>2</sub>.

stannic oxide) exhibit a relatively large inelastic response for maximum effective strains similar to those of Figure 8. The oxide/SWNT-CA composites of SiO<sub>2</sub> and TiO<sub>2</sub> also behave inelastically (Figure 8), whereas SnO<sub>2</sub>/SWNT-CA composites retained very elastic properties of the CNT-based scaffold.

Although elastic properties of aerogels can be, at least qualitatively, related to structure connectivity (i.e., to how the nanoligaments are interconnected into a three-dimensional structure),

the mechanisms of inelastic deformation of aerogels are not understood. Neither is it clear which steps of aerogel preparation have a dominant effect on inelastic properties, and more work is currently needed to understand inelastic deformation of aerogels. Hence, we turn to a more detailed analysis of Young's modulus ( $E$ ) data.

In any analysis of the mechanical deformation behavior of porous solids, the first parameter to consider is the monolith



**Table 1. Physical Properties of SWNT-CA Scaffold, Bulk SiO<sub>2</sub>, SiO<sub>2</sub>/SWNT-CA, Bulk SnO<sub>2</sub>, and SnO<sub>2</sub>/SWNT-CA Composite**

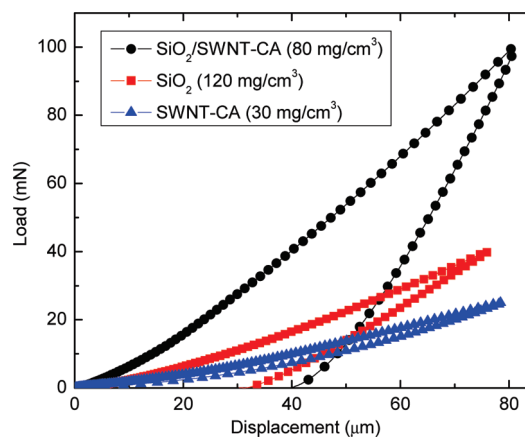
material	CNT (vol %) (wt %)	density (g/cm <sup>3</sup> )	<i>E</i> (MPa)	$\sigma$ (S cm <sup>-1</sup> )
SWNT-CA	1 (55)	0.028	1.2 ± 0.1	1.12
SiO <sub>2</sub>	0	0.120	2.4 ± 0.2	<0.001
SiO <sub>2</sub> /SWNT-CA	1 (16)	0.080	7.3 ± 0.4	1.00
SnO <sub>2</sub>	0	0.204	3.6 ± 1.7	<0.001
SnO <sub>2</sub> /SWNT-CA	1 (33)	0.046	1.0 ± 0.2	1.00

**Table 2. Physical Properties of Bulk TiO<sub>2</sub> and TiO<sub>2</sub>/SWNT-CA Composites (amorphous and crystalline)**

material	CNT (vol %) (wt%)	density (g/cm <sup>3</sup> )	<i>E</i> (MPa)
TiO <sub>2</sub>	0	0.193	3.5 ± 0.2
TiO <sub>2</sub> /SWNT-CA (amorphous)	1 (16)	0.082	17.3 ± 1.7
TiO <sub>2</sub> /SWNT-CA (crystalline)	2 (23)	0.108	14.9 ± 0.7

density because mechanical properties depend superlinearly on the density.<sup>28</sup> Because of differences in the geometry and connectivity of ligaments, different aerogels exhibit different scaling behavior of *E* on the monolith density ( $\rho$ ). In particular, for TMOS-derived base-catalyzed SiO<sub>2</sub> aerogels, as studied in this work, the *E* scales as  $E \sim \rho^{3.7}$ ,<sup>56</sup> whereas for our CNT-based and conventional carbon aerogels,  $E \sim \rho^{2.7}$ .<sup>28</sup> The SiO<sub>2</sub>/SWNT-CA composite aerogel with a monolith density of 80 mg/cm<sup>3</sup> is made of 30 mg/cm<sup>3</sup> of carbon and 50 mg/cm<sup>3</sup> of SiO<sub>2</sub>. The analysis for SiO<sub>2</sub>/CNT composites is further simplified by the fact that the mass densities of ligaments in both aerogels are similar ( $\sim 2$  g/cm<sup>3</sup>). If such a composite aerogel were made from two interpenetrating and not cross-linked networks of carbon and SiO<sub>2</sub> nanoligaments with monolith densities of 30 and 50 mg/cm<sup>3</sup>, the contribution to the elastic modulus from carbon and SiO<sub>2</sub> networks would be  $\sim 1$  and 0.1 MPa, respectively.<sup>28,56</sup> Hence, a much larger Young's modulus of  $\sim 7$  MPa of the SiO<sub>2</sub>/SWNT-CA composite (Table 1) is consistent with electron microscopy observations (Figure 1) that the composite aerogel has morphology of the carbon scaffold with SiO<sub>2</sub> particles decorating carbon ligaments rather than of two interpenetrating but poorly cross-linked SiO<sub>2</sub> and carbon networks.

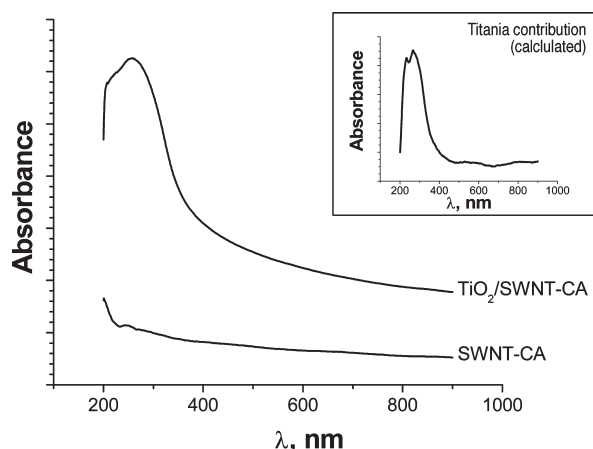
This scaling law analysis could be extended further by noting that a CNT-based aerogel with a density of 80 mg/cm<sup>3</sup> has a Young's modulus of  $\sim 15$  MPa,<sup>28</sup> which is close to the modulus of the SiO<sub>2</sub>/CNT composite ( $\sim 7$  MPa). A factor of 2 lower modulus of the composite could be attributed to significantly weaker atomic bonds in SiO<sub>2</sub> (and, hence, a lower *E*) as compared to the case of graphitic carbon. Indeed, the Young's modulus of full density amorphous silica is  $\sim 70$  GPa as compared to typical  $\sim 200$ – $400$  GPa modulus values for graphitic carbon fibers. Hence, coating of carbon aerogel ligaments with SiO<sub>2</sub> nanoparticles has a mechanical reinforcement effect comparable to that of increasing the density of the carbon scaffold, suggesting good adhesion between the deposited SiO<sub>2</sub> nanoparticles and the SWNT-CA support.

**Figure 8.** Continuous load–displacement curves for the SiO<sub>2</sub>/SWNT-CA composite, SiO<sub>2</sub> aerogel, and SWNT-CA scaffold. Monolith densities are given in the legend.

An even greater increase in the elastic modulus is observed in TiO<sub>2</sub>/SWNT-CA composites, for both amorphous and crystalline (anatase) TiO<sub>2</sub>/SWNT-CA composites (Tables 1 and 2). Because the weight density of full-density TiO<sub>2</sub> is about twice that of graphitic carbon and Young's moduli of full-density TiO<sub>2</sub> and graphitic carbon are similar, a uniform coating of a SWNT-CA scaffold with an initial density of 30 mg/cm<sup>3</sup> with TiO<sub>2</sub> with a volumetric weight density of 50 mg/cm<sup>3</sup> is comparable to a case of a purely carbon nanofoam with a monolithic density of  $\sim 30 + 50 \cdot 2/4 = 55$  mg/cm<sup>3</sup>. According to the *E* scaling behavior for CNT-aerogels,<sup>28</sup> such a carbon aerogel has  $E \sim 6$  MPa, which is three times lower than *E* for the TiO<sub>2</sub>/SWNT-CA composite (Table 2). This could be attributed to additional cross-linking of ligaments by TiO<sub>2</sub> particles as opposed to a less efficient process of a uniform coating of ligaments of the carbon scaffold. The cross-linking effectively changes the connectivity of the ligament network and improves mechanical properties and their scaling behavior.

Table 1 shows that, in contrast to the cases for SiO<sub>2</sub> and TiO<sub>2</sub>, mechanical properties of the SnO<sub>2</sub>/SWNT-CA composite are dominated by those of the CNT scaffold. This difference in reinforcement may be related to different amounts of oxide deposited on the SWNT-CA (33 wt % for SnO<sub>2</sub> vs 70 wt % for SiO<sub>2</sub> and TiO<sub>2</sub>), resulting in an increase of the monolith density by  $\sim 17$  at.% for SnO<sub>2</sub> vs  $\sim 167$  and  $\sim 83$  at.% for SiO<sub>2</sub> and TiO<sub>2</sub>, respectively. Alternatively, such differences could also arise from different interfacial interactions between the deposited oxide and the SWNT-CA support due to the different reaction chemistries used to deposit oxide coatings. Additional studies of deformation behavior of carbon aerogels with variable loading of SnO<sub>2</sub> could provide insight into the structure–property correlation of SnO<sub>2</sub>/SWNT-CA composites.

Composites of TiO<sub>2</sub> and carbon have been shown to exhibit higher photocatalytic activity over a wider absorption band relative to TiO<sub>2</sub> alone. Therefore, we have also measured the UV–vis absorption spectrum of the annealed TiO<sub>2</sub>/SWNT-CA composite as a suspension in ethanol. As shown in Figure 9, the spectrum for the TiO<sub>2</sub>/SWNT-CA material shows not only the well-known TiO<sub>2</sub> absorption band around 260 nm but also absorption far into the visible at 500 nm when the contribution from the CNT scaffold is removed (the inset in Figure 9). This widening of the absorption band in TiO<sub>2</sub>/C composites is



**Figure 9.** UV-vis absorption spectra for TiO<sub>2</sub>/SWNT-CA and SWNT-CA. Spectra are offset for clarity. Inset shows contribution of TiO<sub>2</sub> nanoparticles in TiO<sub>2</sub>/SWNT-CA (SWNT-CA spectrum subtracted).

well-documented in the literature and is another reason why TiO<sub>2</sub>/CNT composites are of such high interest.<sup>57</sup>

## CONCLUSIONS

In summary, novel oxide/CNT nanocomposites were fabricated through the deposition of oxide coatings on monolithic SWNT-CAs supports. Infiltration and deposition of the oxides were achieved with little to no degradation of the extended CNT network of the support, yielding highly conductive nanocomposites. Significant mechanical reinforcement was also observed. In addition, the oxide/CNT nanocomposites exhibited high surface areas and large internal pore volumes. The monolithic nature of these oxide/SWNT-CA assemblies should prove advantageous for a number of applications, such as battery electrodes, sensing devices, and catalysts. These results, along with those for the polymer/SWNT-CA composites, show the versatility and potential of the 3D CNT scaffold approach.

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